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[List of Filed Articles]

[Article Name] Claims 1

[Article Name]	Specification	1
[Article Name]	Abstract	1
[General Power of Attorney No.]	0000937	
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[Name of Document] Claims

[Claim 1]

A lubricating oil composition for sizing press working, comprising (A) a lubricating base oil having a kinematic viscosity of 0.5 to 100 mm<sup>2</sup>/s at 40°C, and compounded therein (B) an extreme-pressure agent in an amount of 0.1 to 10 % by mass and (C) a metal deactivator in an amount of 0.01 to 5 % by mass, each based on a total amount of said composition.

[Claim 2]

A lubricating oil composition for sizing press working according to claim 1, wherein said extreme-pressure agent, being component (B), is an organic phosphoric acid ester compound, and said metal deactivator, being component (C), is a benzotriazole compound and/or a thiadiazole compound.

[Claim 3]

A lubricating oil composition for sizing press working according to claim 1 or 2, further comprising (D) an anti-oxidizing agent and/or an anti-foaming agent.

[Claim 4]

A lubricating oil composition for sizing press working according to claim 2 or 3, wherein said organic phosphoric acid ester compound, being component (B), has a phosphoric acid residue having a total carbon number of 8 or more.

[Claim 5]

A lubricating oil composition for sizing press working

according to any one of claims 2 through 4, wherein said organic phosphoric acid ester compound is a phosphite ester or an acid phosphite ester.

[Claim 6]

A lubricating oil composition for sizing press working according to any one of claims 1 through 5, wherein said lubricating oil composition is used in sizing a sintered alloy for oil impregnated bearings.

[Claim 7]

A method of preparing a sintered, oil impregnated bearing, characterized by sizing press working of a sintered alloy with the use of a lubricating oil composition for sizing press working as described in any one of claims 1 through 6, followed by degreasing and impregnating with a bearing oil.

[Claim 8]

A sintered, oil impregnated bearing prepared by a method according to claim 7.

[Name of Document] Specification

[Title of the Invention] Lubricating oil composition for sizing  
press working

[Technical Field]

[0001]

The present invention relates to a lubricating oil composition for sizing press working and, more specifically, to a lubricating oil composition for use in sizing press working of a sintered metal, particularly for a sintered metal for oil impregnated bearings.

[Background Art]

[0002]

The sintered, oil impregnated bearings are more inexpensive than ball bearings and fluid dynamic bearings and, therefore, are utilized for a number of applications as a substitute for these bearings in electric accessories for automobiles and various electric appliances. The sintered, oil impregnated bearings are generally produced through a compacting step, a sintering step, a sizing press working step, and a cleaning (degreasing) step. In the sizing press working step, a machining oil of a mineral oil has been hitherto used. The known machining oil, however, is unsatisfactory with respect to the machinability because of failure to form sufficient oil films. Further, because of poor degreasing efficiency, the mineral oil-type machining oil tends to remain

in a large amount in the sintered metal. Further, since the remaining oil is poor in compatibility with the impregnated oil and sintered metal used in oil impregnated bearings, generation of sludge is caused.

[0003]

In this circumstance, there is a demand for a lubricating oil for sizing press working which exhibits excellent machinability, degreasing efficiency, and compatibility with the impregnated oil and sintered metal used in oil impregnated bearings. With regard to published documents, Patent Document 1 discloses the use of an oil which is the same as a bearing oil. Patent Document 2 discloses the use of a rapeseed oil. There is, however, a room left for the improvement in the known oils with respect to their performance.

[0004]

[Patent Document 1] JP-A-H06-264110 (page 2)

[Patent Document 2] JP-A-H08-209370 (page 2)

[Disclosure of the Invention]

[Problems to be Solved by the Invention]

[0005]

The present invention has been made in the above-described circumstance and an object of the present invention is to provide a lubricating oil composition for sizing press working which is excellent in machinability and degreasing efficiency and which is excellent in compatibility

with an impregnated oil and a sintered metal used in oil impregnated bearings.

[Means for Solving the Problems]

[0006]

The present inventors have made an intensive study and have found that the object can be effectively achieved by a composition containing a specific, low viscosity lubricating base oil and an extreme-pressure agent and a metal deactivating agent compounded therein in specific amounts. The present invention has been completed on the basis of the above finding.

Thus, the gist of the present invention is as follows:

1. A lubricating oil composition for sizing press working, comprising (A) a lubricating base oil having a kinematic viscosity of 0.5 to 100 mm<sup>2</sup>/s at 40°C, and compounded therein (B) an extreme-pressure agent in an amount of 0.1 to 10 % by mass, and (C) a metal deactivator in an amount of 0.01 to 5 % by mass, each based on a total amount of the composition.
2. A lubricating oil composition for sizing press working as described in 1 above, wherein the extreme-pressure agent, being component (B), is an organic phosphoric acid ester compound and the metal deactivator, being component (C), is a benzotriazole compound and/or a thiadiazole compound.
3. A lubricating oil composition for sizing press working as described in 1 or 2 above, further comprising (D) an anti-oxidizing agent and/or an anti-foaming agent.

4. A lubricating oil composition for sizing press working as described in 2 or 3 above, wherein the organic phosphoric acid ester compound, being component (B), has a phosphoric acid residue having a total carbon number of 8 or more.

5. A lubricating oil composition for sizing press working as described in any one of 2 through 4 above, wherein the organic phosphoric acid ester compound is a phosphite ester or an acid phosphite ester.

6. A lubricating oil composition for sizing press working as described in any one of 1 through 5 above, wherein the lubricating oil composition is used in sizing press working of a sintered alloy for oil impregnated bearings.

7. A method of preparing a sintered, oil impregnated bearing, characterized by sizing press working of a sintered alloy with the use of a lubricating oil composition for sizing press working as defined in any one of 1 through 6 above, followed by degreasing and then impregnating with a bearing oil.

8. A sintered, oil impregnated bearing prepared by a method as described in 7 above.

[Effect of the Invention]

[0007]

According to the present invention a lubricating oil composition for sizing press working which is excellent in machinability, degreasing efficiency, and compatibility with an impregnating oil and a sintered metal used in oil impregnated

bearings may be provided.

[Best Mode for Carrying out the Invention]

[0008]

In the lubricating oil composition for sizing press working according to the present invention, it is essential that a mineral oil and/or a synthetic oil having a kinematic viscosity in the range of 0.5 to 100 mm<sup>2</sup>/s at 40°C be used as a base oil. A viscosity less than 0.5 mm<sup>2</sup>/s is disadvantageous because of a reduction of the strength of oil films and an increase of the loss by evaporation. A viscosity exceeding 100 mm<sup>2</sup>/s is not preferable because of a poor degreasing efficiency. The kinematic viscosity is preferably 0.5 to 40 mm<sup>2</sup>/s, more preferably 0.5 to 10 mm<sup>2</sup>/s.

Various mineral oils are usable. Examples of such mineral oils include distillate oils obtainable by atmospheric distillation of paraffin base crude oils, intermediate base crude oils or naphthene base crude oils, distillate oils obtainable by vacuum distillation of residual oils of the above atmospheric distillation, and refine oils obtainable by refining the above distillate oils in a conventional manner, such as solvent refined oils, hydrogenation refined oils, dewaxed oils and clay treated oils. Above all highly refined mineral oils are preferable from the standpoint of oxidization stability.

[0009]

As the synthetic oil, there may be used, for example, a poly( $\alpha$ -olefin), an olefin copolymer (such as an ethylene-propylene copolymer), a branched olefin such as polybutene, polyisobutylene or polypropylene, a hydrogenated product of the above polymer, further a hydrocarbon synthetic oil such as an alkylbenzene or an alkyl naphthalene. Above all, a hydrogenated product of a branched olefin is preferable.

[0010]

As the base oil in the present invention, the above-described mineral oils may be used singly or in combination of two or more thereof and the above-described synthetic oils may be used singly or in combination of two or more thereof. It is also possible to use one or more mineral oils in conjunction with one or more synthetic oils. The pour point which is an index of the characteristics at low temperatures is not specifically limited but is preferably  $-10^{\circ}\text{C}$  or lower.

[0011]

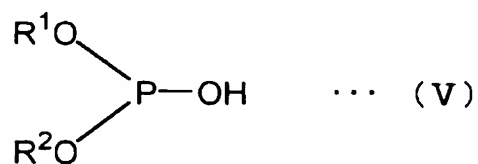
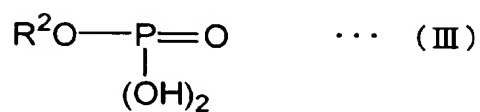
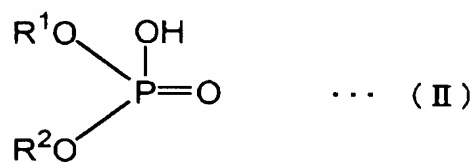
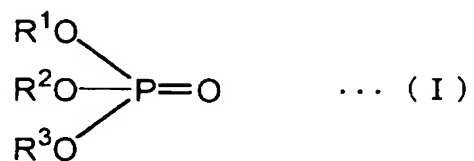
As the extreme-pressure agent which is component (B) of the lubricating oil composition for sizing press working according to the present invention, there may be mentioned, for example, an organic phosphoric acid ester compound.

The organic phosphoric acid ester compound may be a phosphoric acid ester compound including a phosphate ester and an acid phosphate ester, or a phosphorous acid ester compound

including a phosphite ester and an acid phosphite ester, which may be represented by the general formulas (I) through (V) shown below. Above all, the phosphorous acid ester compounds including a phosphite ester and an acid phosphite ester are preferable from the standpoint of degreasing efficiency.

[0012]

[Chemical Formula 1]



[0013]

In the above general formulas (I) through (V),  $R^1$  to  $R^3$  may be same or different and each represent an alkyl group or an alkenyl group having 4 to 30 carbon atoms, an aryl group or an alkylaryl group having 6 to 30 carbon atoms or an aralkyl group having 7 to 30 carbon atoms.

The phosphoric acid residue of the organic phosphoric acid ester compound preferably has a total carbon number of 8 or more. When the total number is 7 or less, there is a possibility that the lubricity is insufficient. The total number is more preferably 12 or more, particularly preferably 18 or more.

The phosphate ester may be an aryl phosphate, an alkyl phosphate, an alkylaryl phosphate, an aralkyl phosphate, an alkenyl phosphate or the like. Examples of the phosphate ester include triphenyl phosphate, tricresyl phosphate, benzyldiphenyl phosphate, ethyldiphenyl phosphate, tributyl phosphate, ethyldibutyl phosphate, cresyldiphenyl phosphate, dicresylphenyl phosphate, ethylphenyldiphenyl phosphate, diethylphenylphenyl phosphate, propylphenyldiphenyl phosphate, dipropylphenylphenyl phosphate, triethylphenyl phosphate, tripropylphenyl phosphate, butylphenyldiphenyl phosphate, dibutylphenylphenyl phosphate, tributylphenyl phosphate, trihexyl phosphate, tri(2-ethylhexyl) phosphate, tridecyl phosphate, trilauryl phosphate, trimyristyl phosphate, tripalmityl phosphate, tristearyl phosphate, and

trioleyl phosphate.

[0014]

Examples of the acid phosphate esters include 2-ethylhexyl acid phosphate, oleyl acid phosphate, tetracosyl acid phosphate, isodecyl acid phosphate, lauryl acid phosphate, tridecyl acid phosphate, stearyl acid phosphate, and isostearyl acid phosphate.

[0015]

Examples of the phosphite esters include tributyl phosphite, triphenyl phosphite, tricresyl phosphite, tri(nonylphenyl) phosphite, tri(2-ethylhexyl) phosphite, tridecyl phosphite, trilauryl phosphite, triisooctyl phosphite, diphenylisodecyl phosphite, tristearyl phosphite, and trioleyl phosphite.

[0016]

Examples of the acid phosphite esters include dibutyl hydrogen phosphite, dilauryl hydrogen phosphite, dioleyl hydrogen phosphite, distearyl hydrogen phosphite, and diphenyl hydrogen phosphite.

[0017]

As the organic phosphoric acid ester compound, it is possible to use a phosphonic acid ester such as dioctyl octylphosphonate, and monoctyl octylphosphonate. Among the organic phosphoric acid ester compounds, tri(2-ethylhexyl) phosphate is preferable as the phosphate ester compound and

dioleoyl hydrogen phosphite is preferable as the phosphite ester compound.

The compounds of component (B) may be used singly or in combination of two or more thereof. The amount of component (B) is chosen from the range of 0.1 to 10 % by mass based on a total amount of the composition. An amount of the component (B) less than 0.1 % by mass causes poor machinability. Too large an amount in excess of 10 % by mass causes poor degreasing efficiency. Preferably, the amount is 0.2 to 5 % by mass, more preferably 0.5 to 3 % by mass.

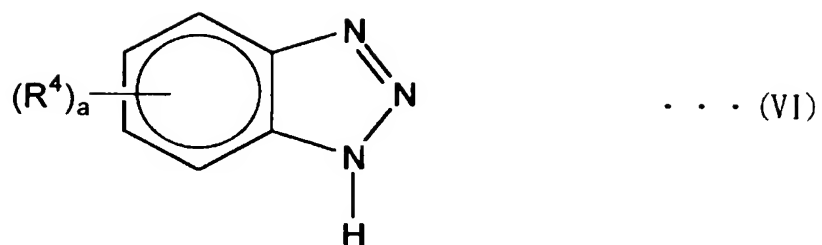
[0018]

As the metal deactivator which is component (C) of the lubricating oil composition for sizing press working according to the present invention, there may be mentioned, for example, a benzotriazole compound and/or a thiadiazole compound.

The benzotriazole compound may be benzotriazole or an alkylbenzotriazole represented by the general formula (VI) shown below, an N-(alkyl)alkylbenzotriazole represented by the general formula (VII) shown below, or an N-(alkyl)aminoalkylbenzotriazole represented by the general formula (VIII) shown below.

[0019]

[Chemical Formula 2]

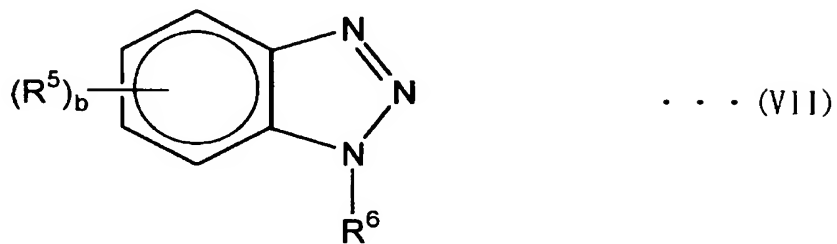


[0020]

wherein  $R^4$  represents an alkyl group having 1 to 4 carbon atoms and  $a$  is an integer of 0 to 4.

[0021]

[Chemical Formula 3]

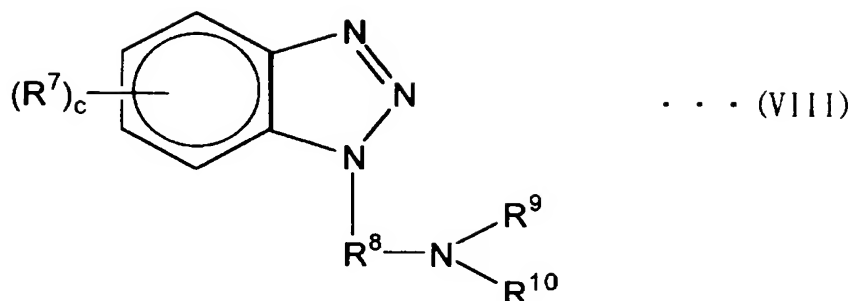


[0022]

wherein  $R^5$  and  $R^6$  are same or different and each represent an alkyl group having 1 to 4 carbon atoms and  $b$  is an integer of 0 to 4.

[0023]

[Chemical Formula 4]



[0024]

wherein  $R^7$  represents an alkyl group having 1 to 4 carbon atoms,  $R^8$  represents a methylene group or an ethylene group,  $R^9$  and  $R^{10}$  are same or different and each represent a hydrogen atom or an alkyl group having 1 to 12 carbon atoms and  $c$  is an integer of 0 to 4.

The symbol  $R^4$  in the above general formula (VI) represents an alkyl group having 1 to 4 carbon atoms, preferably 1 or 2 carbon atoms. Specific examples of the alkyl group include a methyl group, an ethyl group, an n-propyl group, an isopropyl group, an n-butyl group, an isobutyl group, a sec-butyl group, and a tert-butyl group. The symbol  $a$  is an integer of 0 to 4, preferably 0 or 1.

[0025]

The symbols  $R^5$  and  $R^6$  in the above general formula (VII) each represent an alkyl group having 1 to 4 carbon atoms, preferably 1 or 2 carbon atoms. Specific examples of the alkyl group are the same as those of  $R^4$ . The symbol  $b$  is an integer of 0 to 4, preferably 0 or 1.

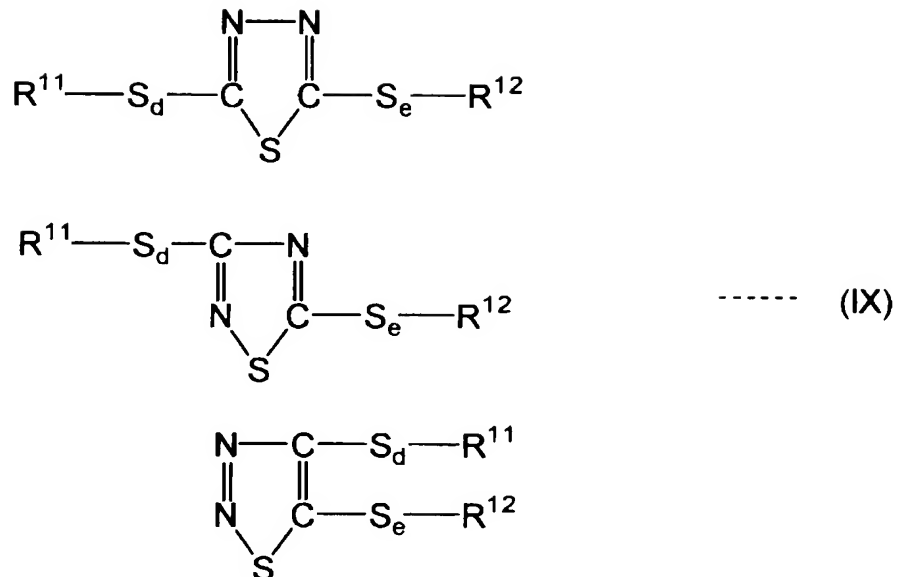
The symbol  $R^7$  in the above general formula (VIII) represents an alkyl group having 1 to 4 carbon atoms, preferably 1 or 2 carbon atoms. Specific examples of the alkyl group are the same as those of  $R^1$ . The symbol  $R^8$  represents a methylene group or an ethylene group, preferably a methylene group. The symbols  $R^9$  and  $R^{10}$  each represent a hydrogen atom, an alkyl group having 1 to 12 carbon atoms, preferably an alkyl group having 1 to 9 carbon atoms. Specific examples of the alkyl group include a methyl group, an ethyl group, an n-propyl group, an isopropyl group, an n-butyl group, an isobutyl group, a sec-butyl group, a tert-butyl group, various pentyl groups, various hexyl groups, various heptyl groups, various octyl groups, various nonyl groups, various decyl groups, various undecyl groups, and various dodecyl groups. The symbol  $c$  is an integer of 0 to 4, preferably 0 or 1.

[0026]

As the thiadiazole compound, there may be preferably used, for example, a 1,3,4-thiadiazole, a 1,2,4-thiadiazole or a 1,4,5-thiadiazole represented by the following general formulas (IX).

[0027]

[Chemical Formula 5]



[0028]

wherein  $\text{R}^{11}$  and  $\text{R}^{12}$  each represent a hydrogen atom or a hydrocarbon group having 1 to 20 carbon atoms, and d and e are each an integer of 0 to 8.

Illustrative of suitable thiadiazole compounds are

- 2,5-bis(n-hexyldithio)-1,3,4-thiadiazole;
- 2,5-bis(n-octyldithio)-1,3,4-thiadiazole;
- 2,5-bis(n-nonyldithio)-1,3,4-thiadiazole;
- 2,5-bis(1,1,3,3-tetramethylbutyldithio)-1,3,4-thiadiazole;
- 3,5-bis(n-hexyldithio)-1,2,4-thiadiazole;
- 3,5-bis(n-octyldithio)-1,2,4-thiadiazole;
- 3,5-bis(n-nonyldithio)-1,2,4-thiadiazole;
- 3,5-bis(1,1,3,3-tetramethylbutyldithio)-1,2,4-thiadiazole;
- 4,5-bis(n-hexyldithio)-1,2,3-thiadiazole;
- 4,5-bis(n-octyldithio)-1,2,3-thiadiazole;

4,5-bis(n-nonyldithio)-1,2,3-thiadiazole; and  
4,5-bis(1,1,3,3-tetramethylbutyldithio)-1,2,3-thiadiazole.  
Above all, 2,5-bis(n-octyldithio)-1,3,4-thiadiazole and  
2,5-bis(n-nonyldithio)-1,3,4-thiadiazole are preferable.

[0029]

Among the metal deactivators of component (C) described  
above, N-substituted benzotriazoles such as  
N-methylbenzotriazole and  
N-dioctylaminomethyl-1,2,3-benzotriazole are preferable from  
the standpoint of compatibility with an impregnating oil and  
lubricity.

The above compounds of the component (C) may be used  
singly or in combination of two or more thereof. The amount  
of the component (C) is 0.01 to 5 % by mass based on a total  
amount of the composition. An amount of the component (C) less  
than 0.01 % by mass causes poor machinability. Too large an  
amount in excess of 5 % by mass causes poor degreasing  
efficiency. Preferably, the amount is 0.03 to 3 % by mass.

[0030]

In the lubricating oil composition for sizing press  
working according to the present invention, an anti-oxidizing  
agent and/or an anti-foaming agent, being a component (D), may  
be additionally used, if necessary.

As the anti-oxidizing agent, there may be mentioned an  
amine-type anti-oxidizing agent, a phenol-type anti-oxidizing

agent, a sulfur-type anti-oxidizing agent or the like.

As the amine-type anti-oxidizing agent, there may be mentioned a monoalkyldiphenylamine-series such as monooctyldiphenylamine or monononyldipheylamine, a dialkyldiphenylamine-series such as 4,4'-dibutyldiphenylamine, 4,4'-dipentyldiphenylamine, 4,4'-dihexyldiphenylamine, 4,4'-diheptyldiphenylamine, 4,4'-dioctyldiphenylamine or 4,4'-dinonyldiphenylamine, a polyalkyldiphenylamine-series such as tetrabutyldiphenylamine, tetrahexyldiphenylamine, tetraoctyldiphenylamine or tetranonyldiphenylamine, or a naphthylamine-series such as  $\alpha$ -naphthylamine, phenyl- $\alpha$ -naphthylamine, butylphenyl- $\alpha$ -naphthylamine, pentylphenyl- $\alpha$ -naphthylamine, hexylphenyl- $\alpha$ -naphthylamine, heptylphenyl- $\alpha$ -naphthylamine, octylphenyl- $\alpha$ -naphthylamine, or nonylphenyl- $\alpha$ -naphthylamine. Above all, the dialkyldiphenylamine-series is preferable. The above amine-type anti-oxidizing agents may be used singly or in combination of two or more thereof.

[0031]

The phenol-type anti-oxidizing agent may be, for example, a monophenol-series such as 2,6-di-tert-butyl-4-methylphenol or 2,6-di-tert-butyl-4-ethylphenol, a diphenol-series such as 4,4'-methylenebis(2,6-di-tert-butylphenol) or 2,2'-methylenebis(4-ethyl-6-tert-butylphenol), or a

polymer-type phenol-series such as tetrakis[methylene-3-(3,5-di-tert-butyl-4-hydroxyphenyl)propionate]methane. The above phenol-type anti-oxidizing agents may be used singly or in combination of two or more thereof.

[0032]

As the sulfur-type anti-oxidizing agent, there may be mentioned phenothiazine, pentaerythritol tetrakis(3-laurylthiopropionate), bis(3,5-tert-butyl-4-hydroxybenzyl)sulfide, thiodiethylenebis(3-(3,5-di-tert-butyl-4-hydroxyphenyl)propionate, 2,6-di-tert-butyl-4-(4,6-bis(octylthio)-1,3,5-triazine-2-methylamino)phenol or the like. These sulfur-type anti-oxidizing agents may be used singly or in combination of two or more thereof.

The above various types of anti-oxidizing agents may be used in combination of two or more thereof.

The amount of the anti-oxidizing agent is in the range of 0.01 to 10 % by mass based on a total amount of the composition, preferably 0.03 to 5 % by mass.

[0033]

As the anti-foaming agent, a liquid silicone is suitably used. For example, methyl silicone, fluorosilicone or polyacrylate may be used.

The amount of the anti-foaming agent is 0.0005 to 0.01 % by mass based on a total amount of the composition.

In the lubricating oil composition for sizing press working according to the present invention, an additive or additives such as a friction controlling agent, a cleaning dispersant, a viscosity index improver and a thickener may be compounded, if necessary, as long as the objects of the present invention are not adversely affected.

[Examples]

[0034]

The present invention will be further described with regard to examples but is not restricted to the examples in any way.

Examples 1 to 8 and Comparative Examples 1 to 6

(1) Preparation of a lubricating oil composition for sizing press working:

To the lubricating base oil shown in Table 1, components shown in Table 1 were compounded in amounts (% by mass) shown in Table 1 on the basis of the total amount of the composition, thereby to prepare lubricating oil compositions for sizing press working.

(2) Evaluation tests as lubricating oil for sizing press working:

The lubricating oil compositions for sizing press working thus prepared were subjected to evaluation tests in

the manner shown below. The results are shown in Table 1.

[0035]

(a) Lubricity test (JASO pendulum test)

In accordance with JASO M-314 6.13, the test was performed at room temperature to determine the coefficient of friction.

(b) Degreasing test

A sintered metal impregnated with the oil was subjected to extraction with n-hexane. The residual amount of the oil in the sintered metal after the extraction was measured.

(c) Compatibility test with an oil for impregnation

An impregnation oil and the sizing oil were mixed in a 1:1 (mass ratio) proportion and the mixture was stored for one month at a room temperature. Presence or absence of precipitates was checked to evaluate stability of the mixture with the impregnation oil.

(d) Compatibility test with a sintered metal

A sintered metal was immersed in the sizing oil and stored at room temperature for one month. The presence or absence of color change of the sintered metal, appearance of the oil, and presence or absence of precipitates were evaluated.

[0036]

[Table 1]

Table 1-1

		Ex. 1	Ex. 2	Ex. 3	Ex. 4	Ex. 5	Ex. 6	Ex. 7	Ex. 8
Amount (% by mass)	Base oil	A1	91	95.5	97.8	98.9	96.9		
		A2							96.9
		A3							
		A4					95	99.45	
		A5							
	Extreme pressure agent	B1	8	4	2	1	3		3
		B2						2	
		B3							
		B4							
	Metal deactivator	C1	1	0.5	0.2	0.1	0.1	0.1	
		C2							
		C3							0.1
Lubricity	JASO pendulum Test	0.093	0.097	0.106	0.111	0.103	0.105	0.112	0.117
Degreasing efficiency	Degreasing Test	0.0057	0.0023	0.0012	0.0006	0.0017	0.0125	0.0516	0.0014
Compatibility	Compatibility with impregnation oil	none	none	none	none	none	none	none	none
	Compatibility with sintered metal	none	none	none	none	none	none	none	none
	Appearance of oil	good	good	good	good	good	good	good	good

[0037]

[Table 2]

Table 1-2

			Comp. Ex. 1	Comp. Ex. 2	Comp. Ex. 3	Comp. Ex. 4	Comp. Ex. 5	Comp. Ex. 6
Amount (% by mass)	Base oil	A1	99.945	84	90		94.9	94.9
		A2						
		A3						
		A4						
		A5				96.9		
	Extreme pressure agent	B1	0.05	15	4	3		
		B2						
		B3					5	
		B4						5
	Metal deactivator	C1	0.005	1		0.1	0.1	
		C2			6			0.1
		C3						
Lubricity	JASO pendulum Test	Coefficient of friction	0.135	0.093	0.107	0.101	0.142	0.11
Degreasing efficiency	Degreasing Test	Residual amount of Oil (g)	0.0003	0.0128	0.116	0.172	0.0198	0.0015
Compatibility	Compatibility with impregnation oil	Precipitates	none	none	form	none	form	form
	Compatibility with sintered metal	Color change	none	none	none	none	change	change
		Appearance of oil	good	discolor	Precipitate	good	discolor	discolor

[0038]

(Remarks)

Components of lubricating oil composition:

A1: Hydrogenated product of polyisobutene; Kinematic viscosity: 1.25 mm<sup>2</sup>/s at 40°C

A2: Naphthene base mineral oil; Kinematic viscosity: 0.98 mm<sup>2</sup>/s at 40°C; Sulfur content: 10 ppm or less

A3: Paraffin base mineral oil; Kinematic viscosity: 8.38 mm<sup>2</sup>/s at 40°C. Sulfur content: 10 ppm or less

A4: Alkylbenzene; Kinematic viscosity: 56 mm<sup>2</sup>/s at 40°C

A5 (comparative): Paraffin base mineral oil; Kinematic viscosity: 131 mm<sup>2</sup>/s at 40°C. Sulfur content: 950 ppm  
[0039]

B1: Dioleoyl hydrogen phosphite

B2: Tri(2-ethylhexyl) phosphate

B3 (comparative): Dioctylpolysulfide

B4 (comparative): ZnDTP

C1: N-dioctylaminomethyl-1,2,3-benzotriazole

C2: Benzotriazole

C3: 2,5-bis(n-nonyldithio)-1,3,4-thiadiazole

[Industrial Applicability]

[0040]

The sintered, oil impregnated bearing may be prepared by sizing press working of a sintered alloy with the use of the lubricating oil composition for sizing press working according to the present invention, followed by degreasing and impregnating with a bearing oil.

[Name of Document] Abstract

[Abstract]

[Problem] A lubricating oil composition for sizing press working which is excellent in machinability and degreasing efficiency and which is excellent in compatibility with an impregnated oil and a sintered metal used in oil impregnated bearings, is provided.

[Means for Resolution] A lubricating oil composition for sizing press working, comprising (A) a lubricating base oil having a kinematic viscosity of 0.5 to 100 mm<sup>2</sup>/s at 40°C, and compounded therein (B) an extreme-pressure agent in an amount of 0.1 to 10 % by mass, and (C) a metal deactivator in an amount of 0.01 to 5 % by mass, each based on a total amount of the composition.

[Selected Drawing] None